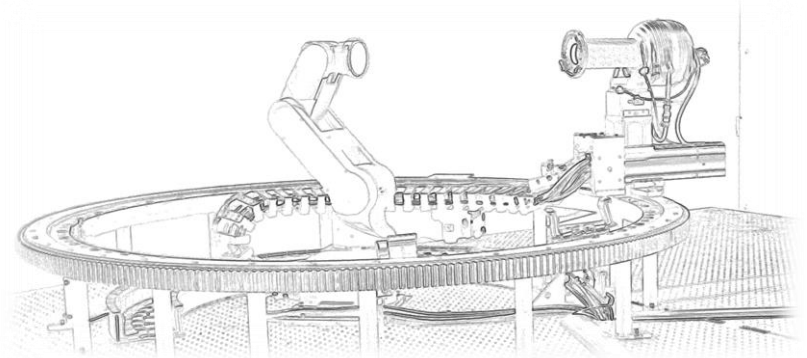
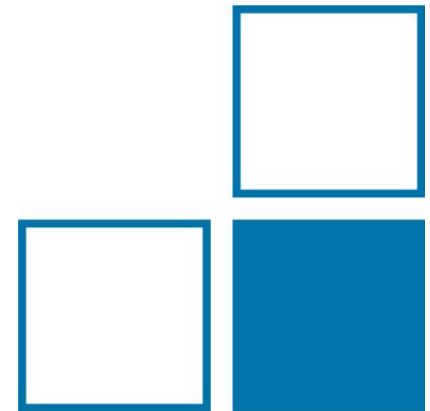


BxDiff WP1:

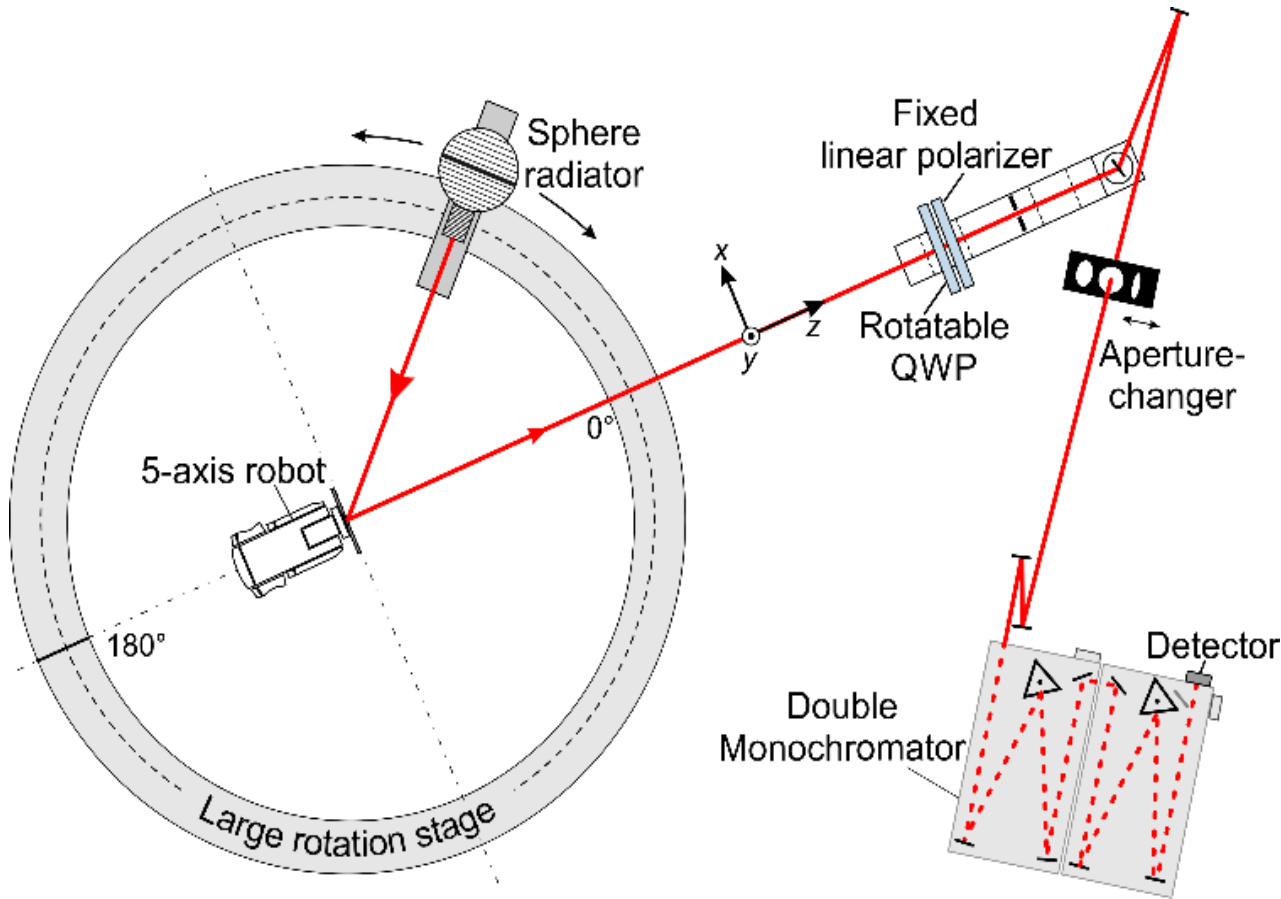
Remarks on uncertainty determination for BxDiff-BRDF comparison measurements



Alfred Schirmacher, Tatjana Quast,
Irina Santourian, Kai-Olaf Hauer



Remarks on uncertainty determination...



radiator-based approach

$$\beta(\lambda) = \frac{L_r(\lambda)}{L_r^{PRD}(\lambda)}$$

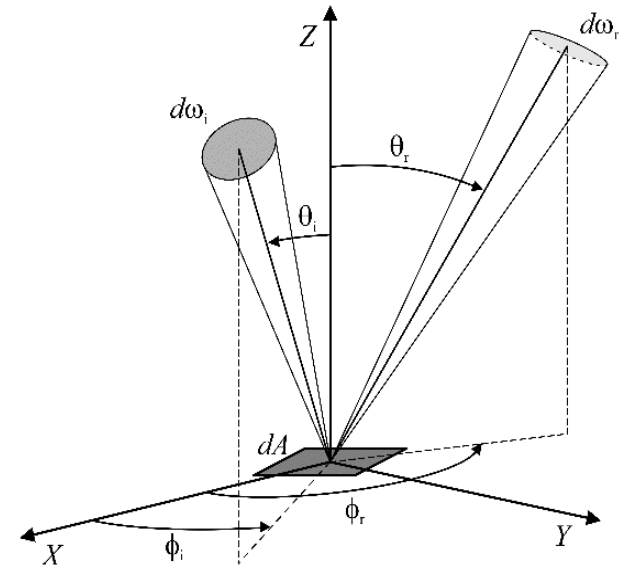
spectral radiance factor

Fig.1 Robot-based Goniometer at PTB

Remarks on uncertainty determination...

$$\beta(\theta_i, \Phi_i, \theta_r, \Phi_r, \lambda) = \frac{L_r(\theta_i, \Phi_i, \theta_r, \Phi_r, \lambda)}{L_r^{PRD}(\theta_i, \Phi_i, \theta_r, \Phi_r, \lambda)}$$

$$\beta(\lambda) = \frac{\pi R^2}{A_Q \cos(\theta_i)} \cdot \frac{S_r(\lambda) - S_{rd}(\lambda)}{S_i(\lambda) - S_{id}(\lambda)}$$



Model for uncertainty calculation

$$\beta(\lambda, R, A_Q, \Delta T, \vec{\Delta}, \vec{\Gamma}, \vec{K}, \vec{C}_{\text{sens}}, \vec{S}, T_f, f_{br}, f_{bi}, f_{pol}, f_{\text{fluo}})$$

$$= \frac{\pi R^2}{A_Q(\Delta T) \cos(\theta_i(\vec{\Delta}, \vec{\Gamma}, \vec{K}))} \cdot T_f \cdot f_{pol}$$

$$\cdot \frac{(c_{\text{sens } 11} + c_{\text{sens } 12})S_r \cdot f_{br} \cdot f_{\text{fluo}} - (c_{\text{sens } 21} + c_{\text{sens } 22})S_{rd}}{f_{bi} \cdot (S_{i1} + S_{i2}) - (c_{\text{sens } 31}S_{id1} + c_{\text{sens } 32}S_{id2})}$$



described in detail in

Metrologia



PAPER • OPEN ACCESS

Uncertainty budget for PTB's gonioreflectometers and ways to improve it in the short VIS spectral range

Irina Santourian^{2,1} , Tatjana Quast¹ and Alfred Schirmacher¹ 

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[Metrologia](#), [Volume 59](#), [Number 2](#)

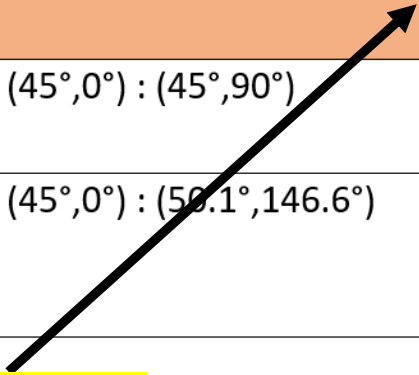
Citation Irina Santourian *et al* 2022 *Metrologia* **59** 025004

Development of an LED-radiator, description and reduction of uncertainty budget in short VIS

Remarks on uncertainty determination...

Geometry- and sample-specific aspects

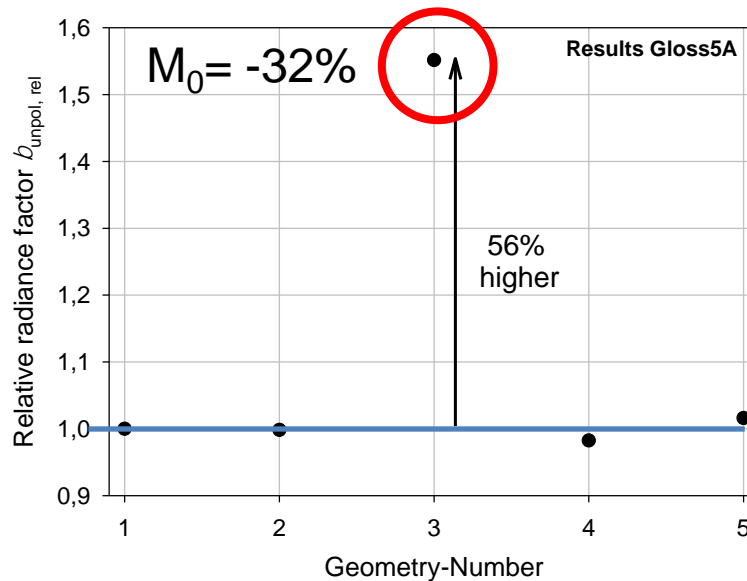
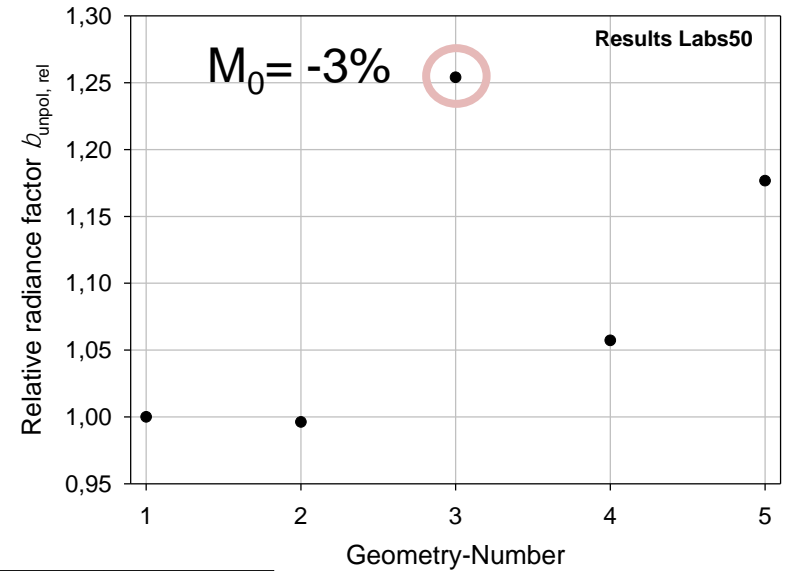
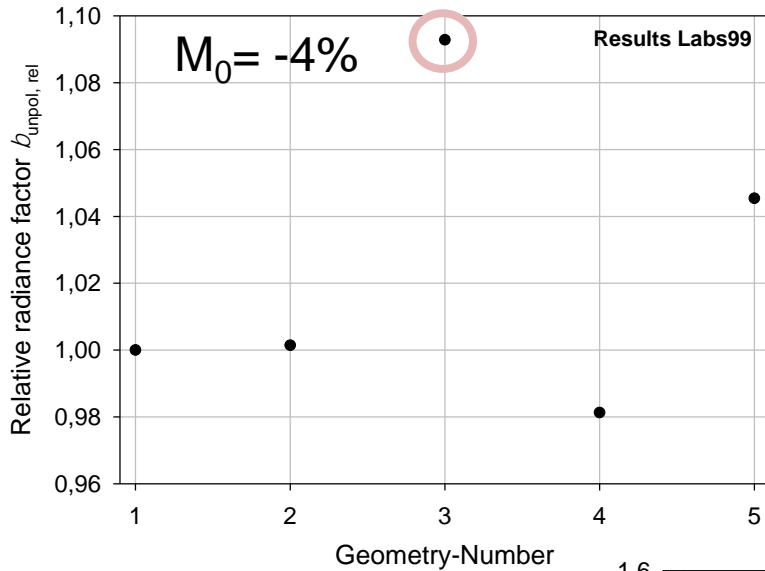
Name / designation		Angle settings	Relative targeted uncertainty (k=2)
in plane	Geo1	(45°,0°) : (0°,0°)	0.1% unrealistic, too small
	Geo2	(0°,0°) : (45°,180°)	
	Geo3	(45°,0°) : (60°,180°) Sample Gloss5A	
out-of-plane	Geo4	(45°,0°) : (45°,90°) unusual geometry	< 4% too high ?
	Geo5	(45°,0°) : (50.1°,146.6°) Sample Gloss5A unusual geometry	



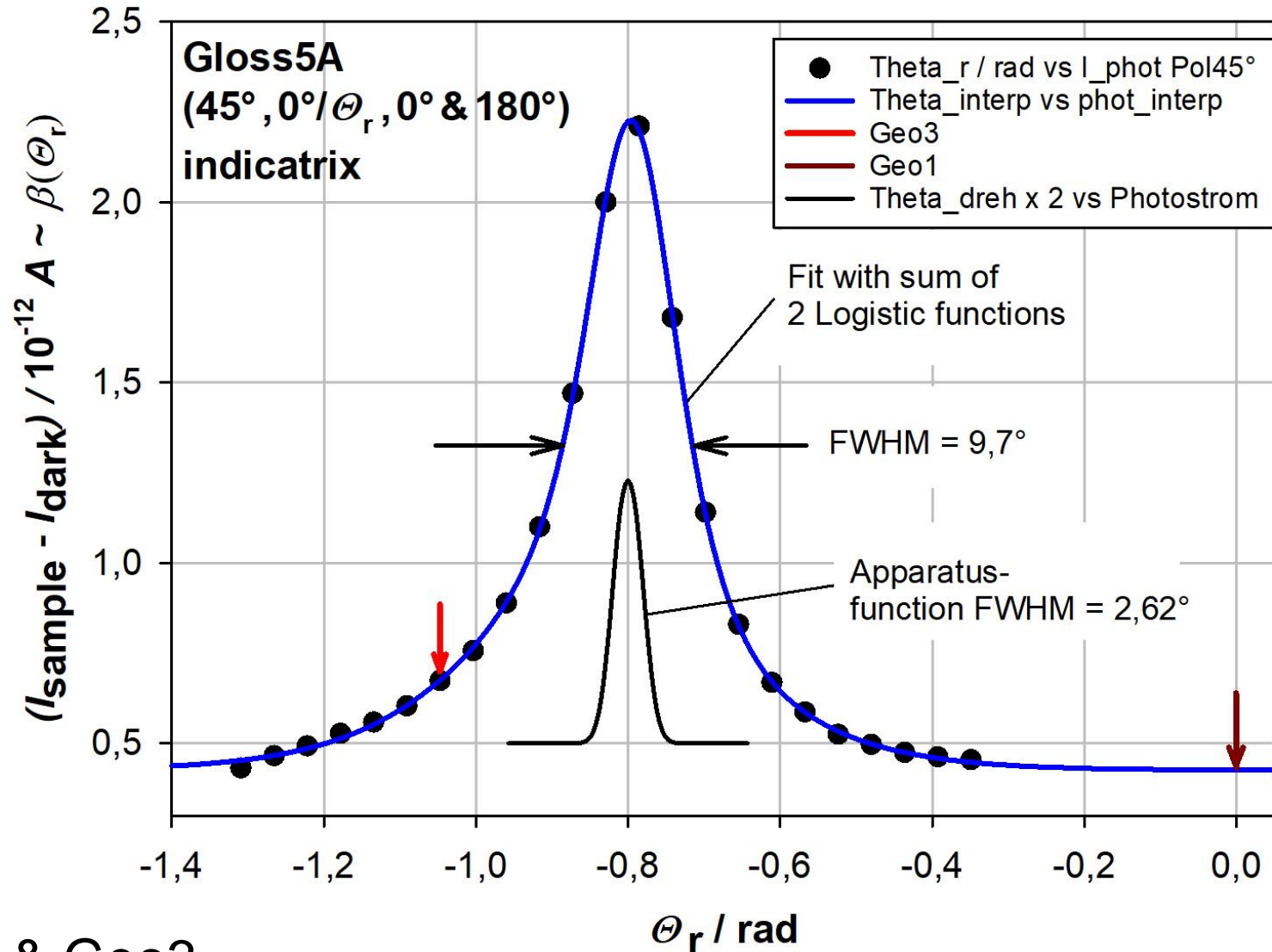
close to specular:

- highly polarised, - convolution error for apparatus function,
- highly sensitive to robot angle positioning

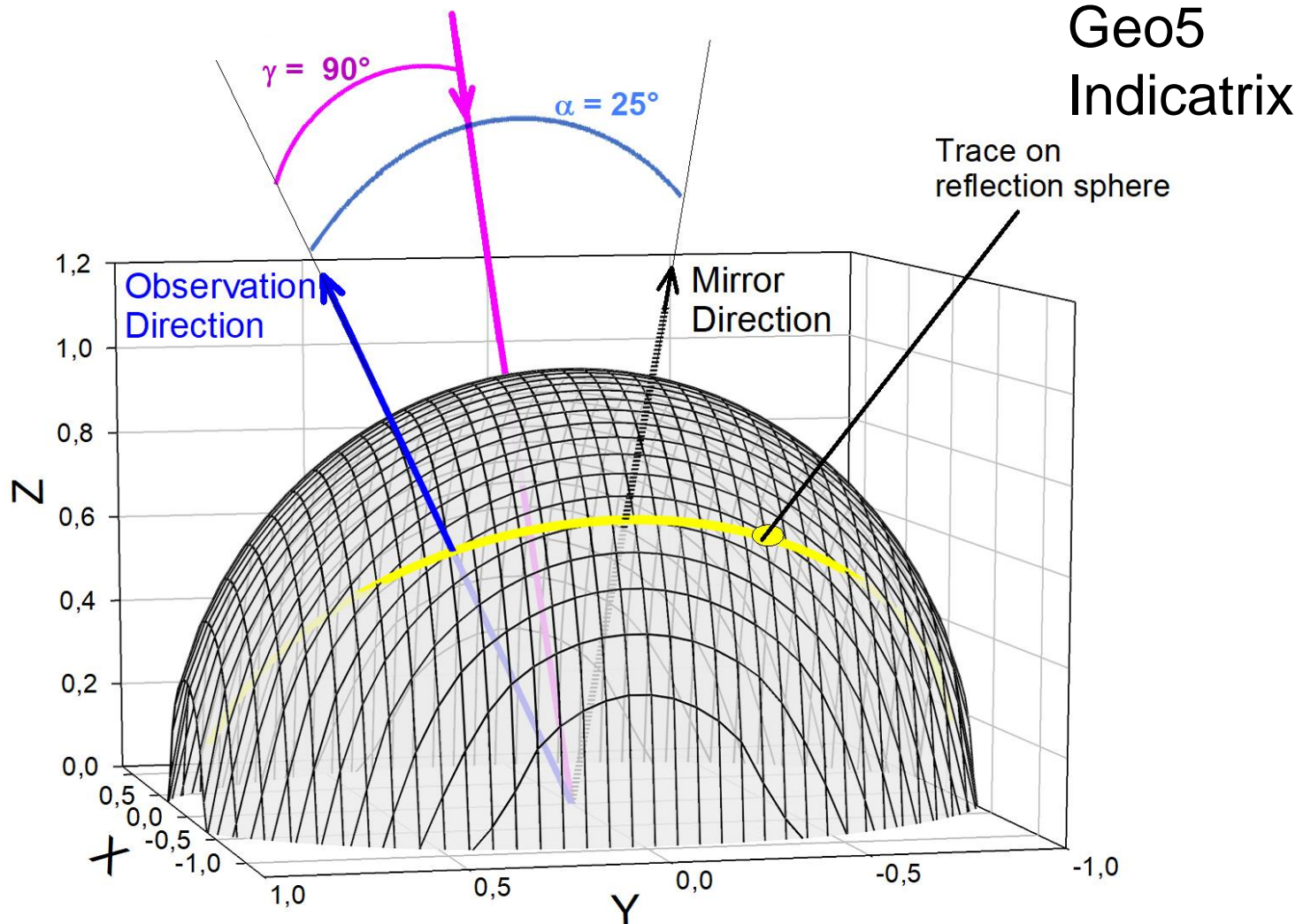
Remarks on uncertainty determination...



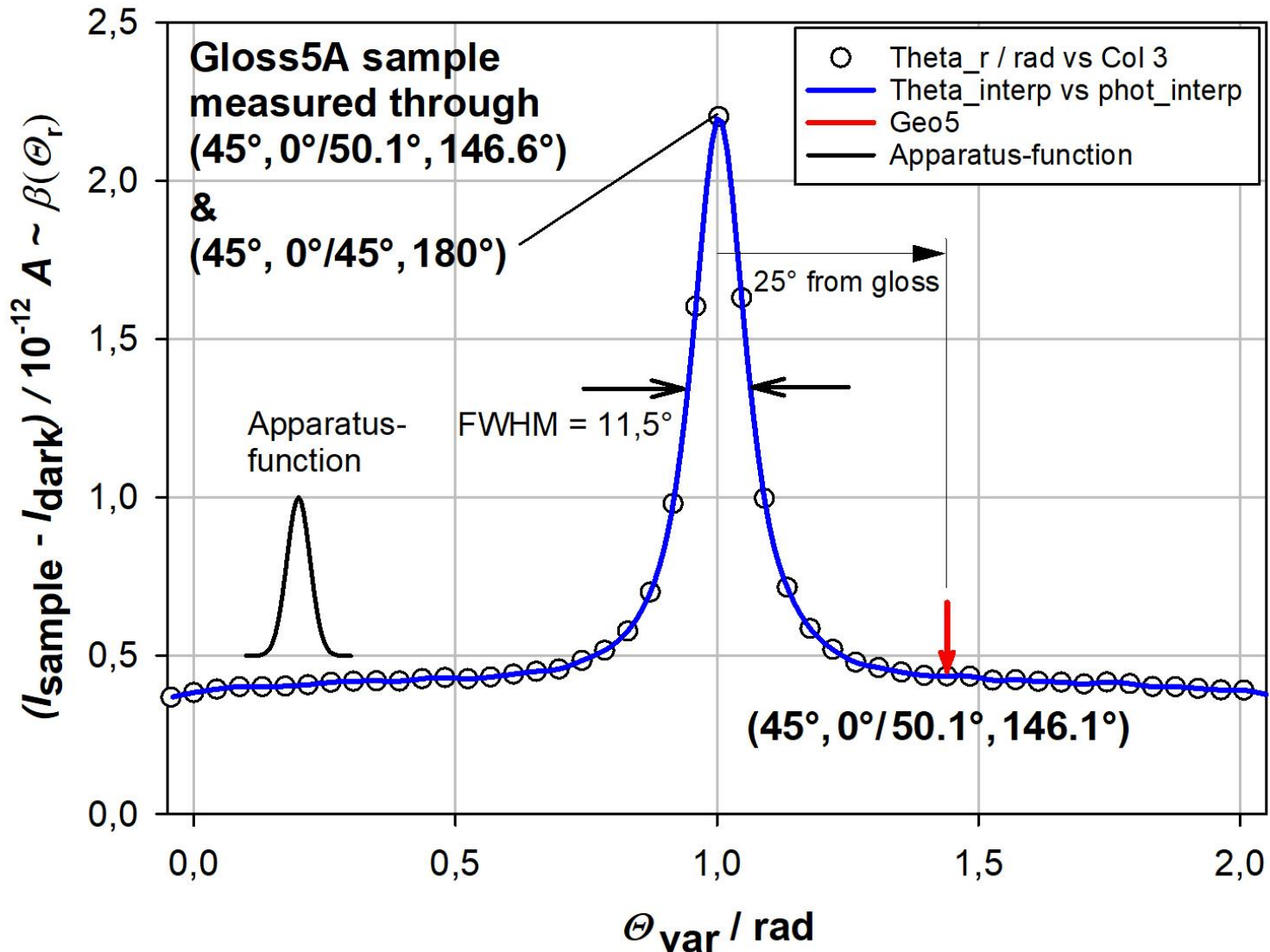
Remarks on uncertainty determination...



Geo1 & Geo3

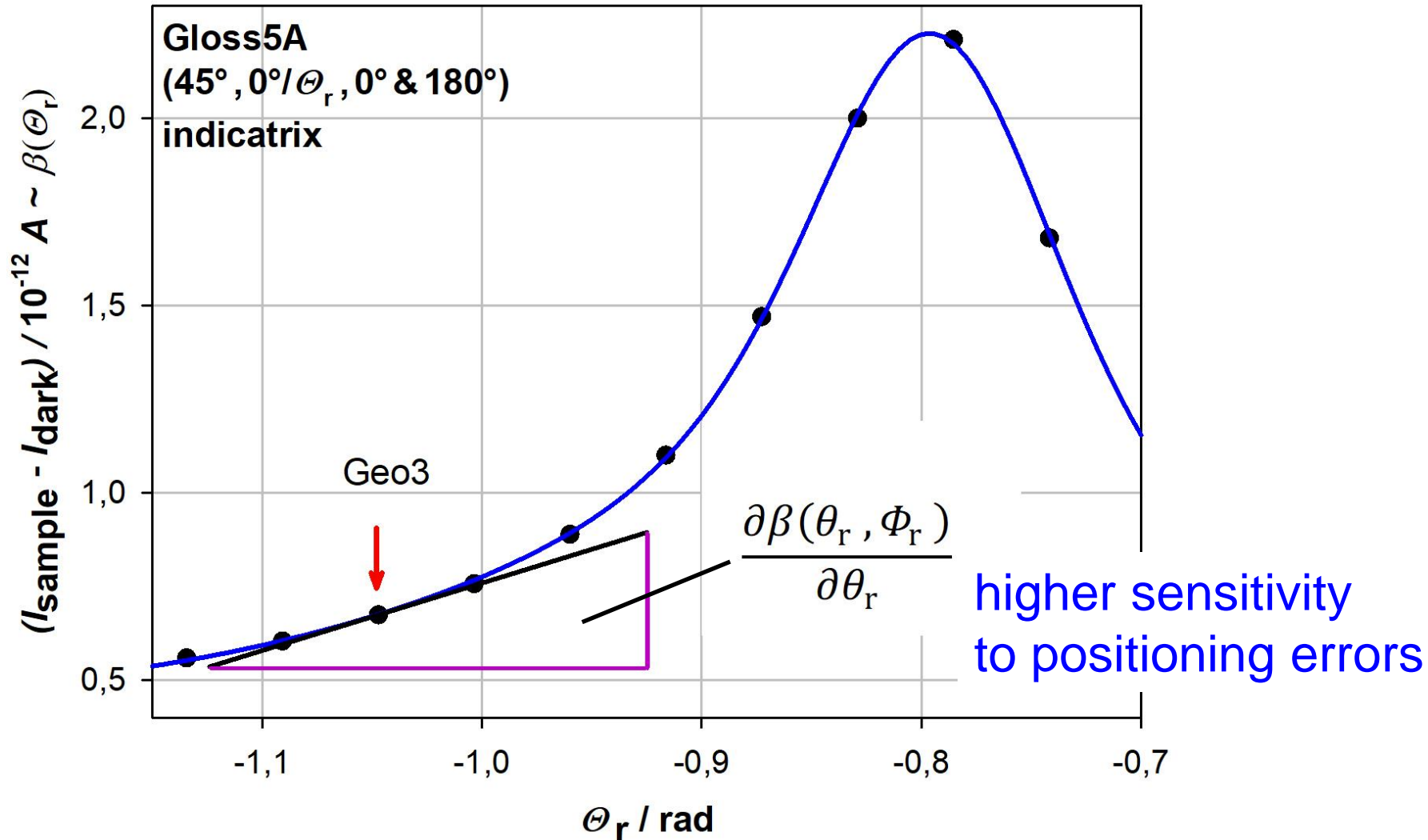


Remarks on uncertainty determination...



Geo5

Remarks on uncertainty determination...

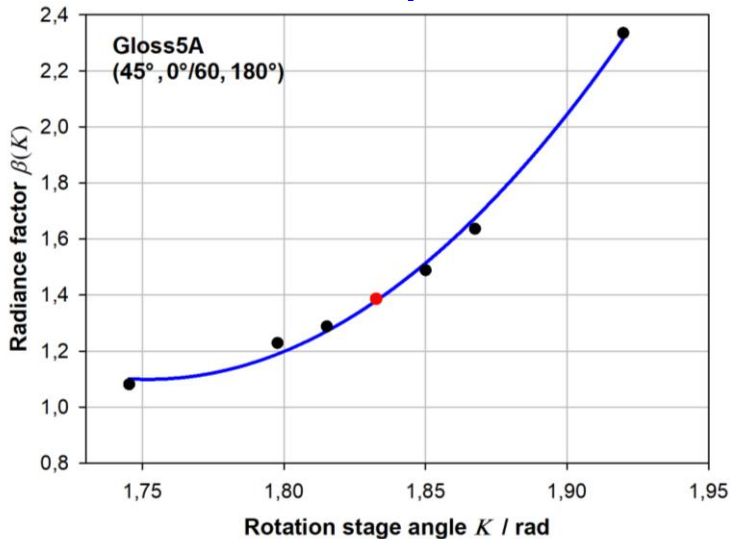


Remarks on uncertainty determination...

Geometry determined by system
(rotation stage & robot) - coordinates

$$\beta = \beta(\theta_i(\vec{\Delta}, \vec{\Gamma}, \vec{K}))$$

Get **sensitivity coefficients** by variation of system - coordinates around the specific measurement geometry



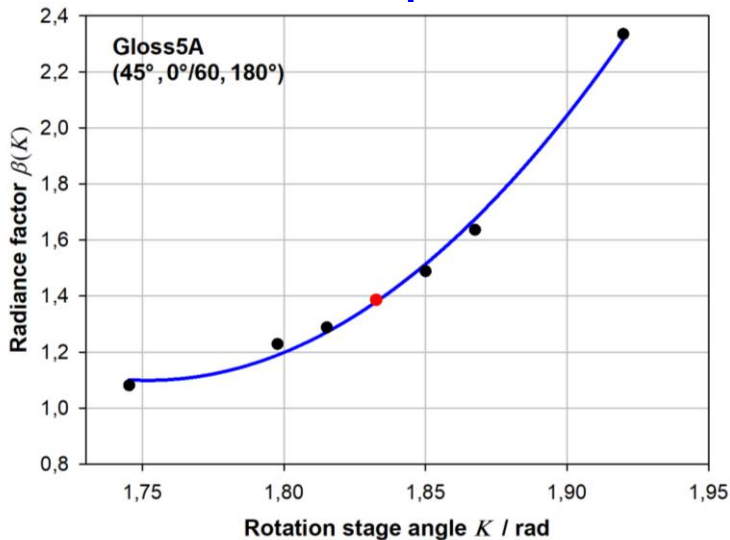
$\frac{\partial \beta}{\partial K} = 6.96 \text{ rad}^{-1}$	Gloss5A Geo3
0.125 rad^{-1}	Labs99 Geo3
0.05 rad^{-1}	Labs99 Geo1

Remarks on uncertainty determination...

Geometry determined by system
(rotation stage & robot) - coordinates

$$\beta = \beta(\Theta_i(\vec{\Delta}, \vec{\Gamma}, \vec{K}))$$

Get **sensitivity coefficients** by variation of system - coordinates around the specific measurement geometry



system-movements **are correlated**

e.g.

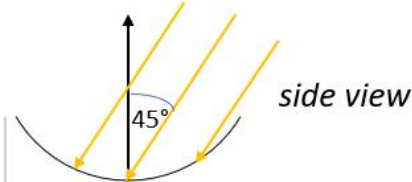
in-plane geometries Geo1 to Geo3

$$r(\Delta, K) = 1$$

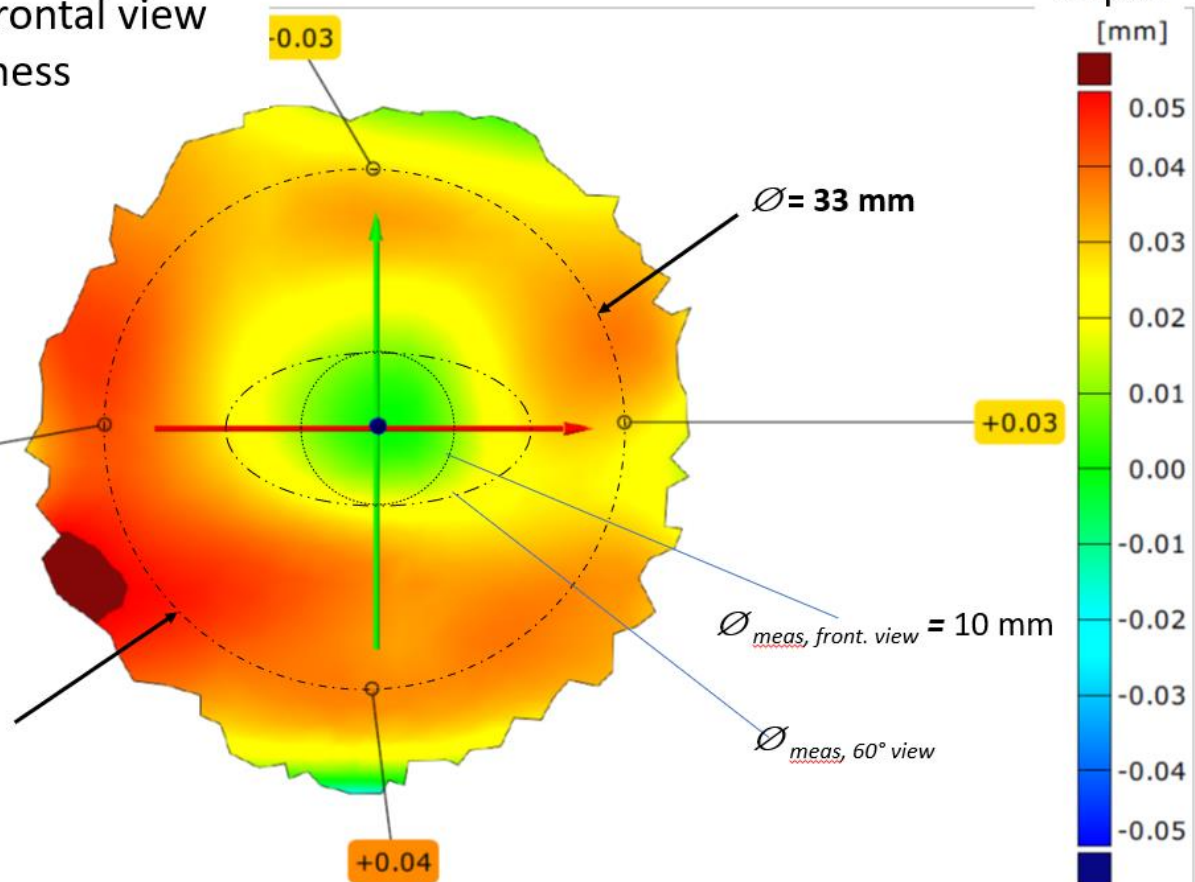
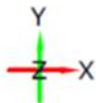
Remarks on uncertainty determination...

Labs50 Adjustment Surface to pivot point
fringe projection scanner / frontal view
accounting for sample thickness

bowl shaped sample

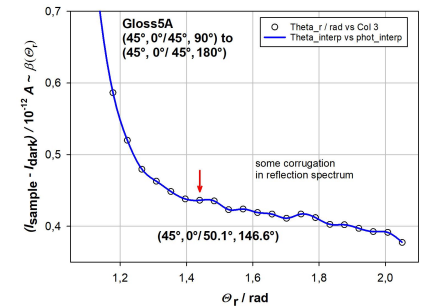
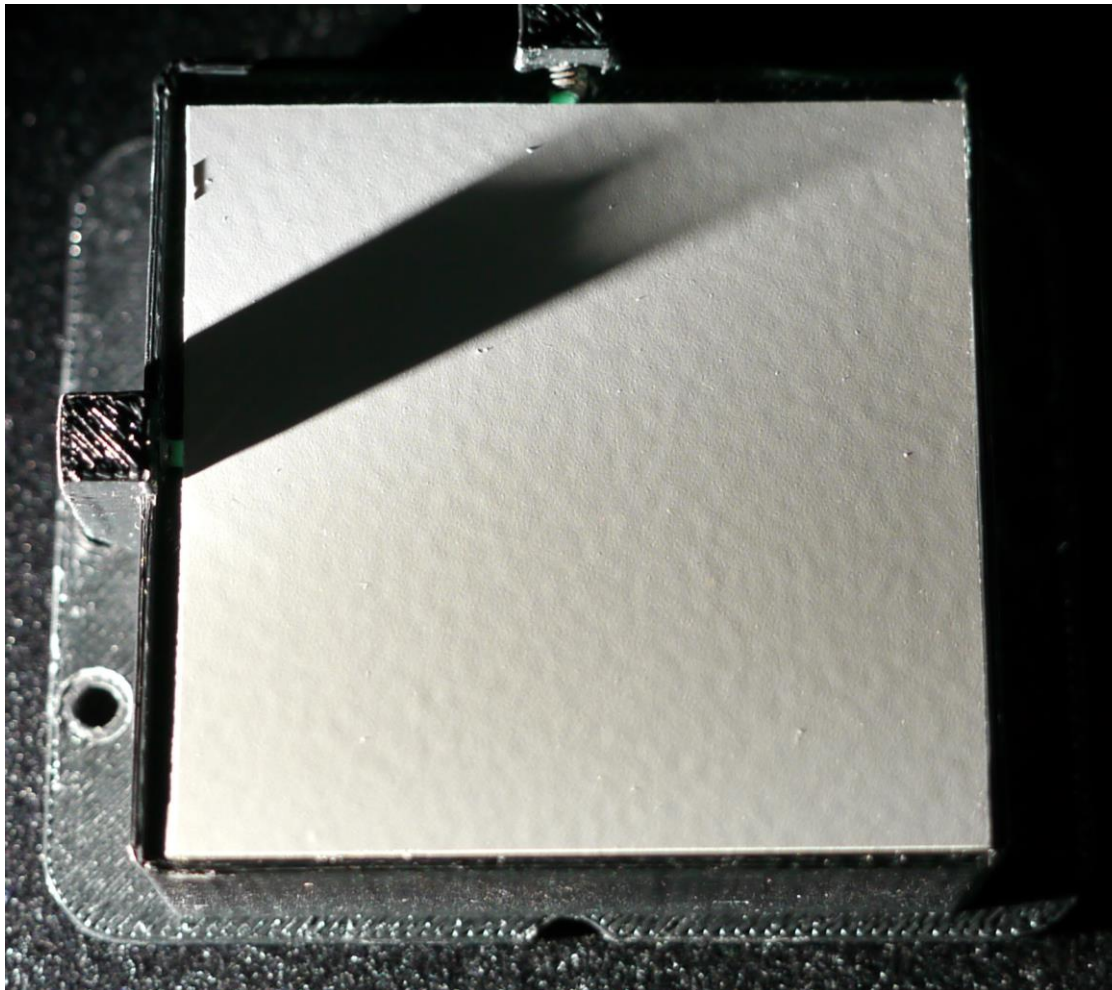


+0.04



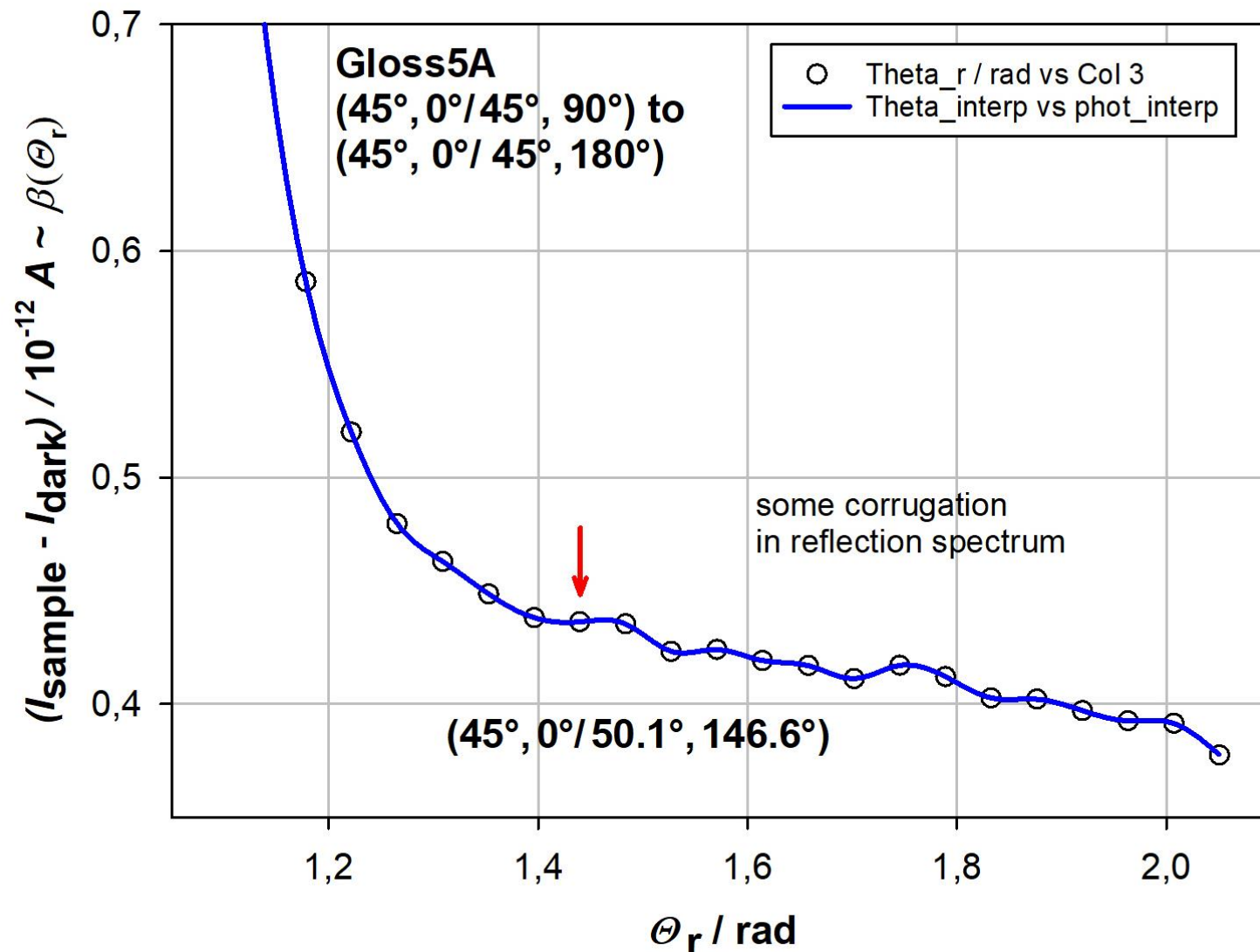
Labs50: Bowl shape not considered because of small spot

Remarks on uncertainty determination...

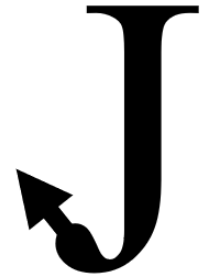
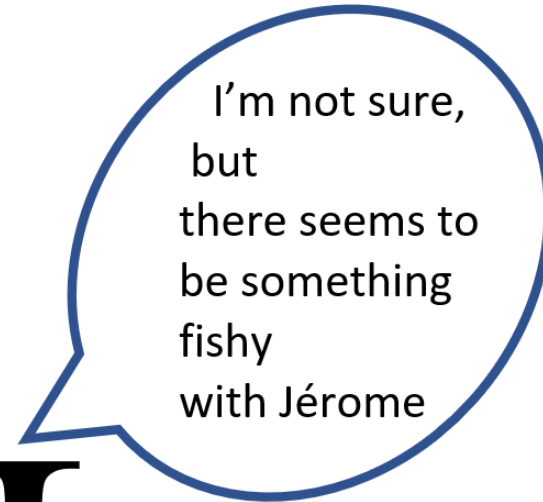


Gloss5A: Some waviness of surface / causes add. uncertainty

Remarks on uncertainty determination...



Uncertainty,
a common problem



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